

METHOD AND DEVICE FOR EFFECTING A COMPUTER-AIDED ESTIMATION OF  
THE MASS OF A VEHICLE, PARTICULARLY OF A COMMERCIAL VEHICLE

FIELD OF THE INVENTION

The present invention relates to a method and a device for effecting a computer-aided estimation of the mass of a vehicle, e.g., of a commercial or goods-carrying vehicle.

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BACKGROUND INFORMATION

In electronic vehicle systems such as electronic stability programs (ESP) for regulating driveability in the extreme range from the standpoint of driving dynamics, or in electronically regulated brake systems (EBS) for commercial vehicles, a value is generally needed for the mass of the vehicle. Since as a rule, no sensors are present for ascertaining the mass, the vehicle mass must be calculated or estimated by suitable algorithms.

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German Published Patent Application No. 42 28 413 describes a method for determining the vehicle mass, in which two longitudinal vehicle accelerations at at least two different points of time and the propulsive powers existing at these points of time are measured. The vehicle mass is then determined from the difference between the propulsive powers and the difference between the longitudinal accelerations.

According to German Published Patent Application No. 198 02 630, to determine the vehicle mass, the propulsive power and the corresponding longitudinal vehicle acceleration are measured at points of time continually following each other with constant time intervals.

U.S. Patent No. 6,347,269 describes ascertaining the vehicle mass on the basis of the propulsive powers, the running

resistances and the vehicle acceleration, the influence of the roadway inclination being eliminated by a high-pass filter.

According to PCT International Published Patent Application No. WO 00/11439, to ascertain the vehicle mass, at least two time-staggered measurements are determined, including one tractive-force variable and one movement variable of the vehicle, one of the two measurements being carried out during a phase free of tractive force, and the other during a tractive-force phase.

In German Published Patent Application No. 101 44 699, a method is described which is based on the equilibrium relationship or ratio between the motive or driving force on one hand, and the accelerative force and the climbing resistance. This equilibrium relationship reads:

$$F = m \cdot (a + g \cdot \sin \alpha) \quad (1)$$

where

F = motive force

a = time derivation of the longitudinal vehicle velocity

$\alpha$  = gradient angle of the roadway

g = gravitational acceleration

m = vehicle mass

In equation (1), the accelerative force is represented by the product  $m \cdot a$ , and the climbing resistance by the product  $m \cdot g \cdot \sin \alpha$ . To calculate mass m of the vehicle, equation (1) is therefore solved for m, and the instantaneous values for F, a and  $\alpha$  are determined from measured quantities. Since gradient angle  $\alpha$  of the roadway being traveled at any one time is not known, as a rule it is estimated with the aid of a computer during coupling phases or during phases without or with very low motive force, or is disregarded altogether. When using converter clutches or powershift transmissions, however, such

freewheeling phases are no longer available, so that a sufficiently accurate estimation of the vehicle mass may be difficult.

## 5 SUMMARY

An example embodiment of the present invention may provide a method for effecting a computer-aided estimation of mass  $m$  of a vehicle such that the above-indicated disadvantages may be avoided. An example embodiment of the present invention may  
10 provide a device for the application of the method.

## DETAILED DESCRIPTION

An example embodiment of the present invention may include evaluating changes in the operating state of the vehicle over  
15 time  $t$  for estimating the vehicle mass. When a vehicle is traveling along any route, gradient angle  $\alpha$  of the roadway is a function of time  $t$ . If one differentiates equation (1) with respect to time  $t$ , the following equation results:

$$\dot{F} = m \cdot (\dot{a} + g \cdot \dot{\alpha} \cdot \cos \alpha) \quad (2)$$

20 Assuming the change in gradient angle  $\alpha(t)$  is very small in time interval  $dt$  considered, the influence of gradient angle  $\alpha(t)$  may be minimized or eliminated. Then  $\dot{\alpha} = d\alpha/dt \approx 0$  applies, and equation (2) reads as follows:

$$25 \quad \dot{F} = m \cdot \dot{a} \quad (3)$$

Due to the time derivation of equation (2), it may therefore be possible to eliminate the influence of gradient angle  $\alpha$ , assumed to be constant for a time, in equation (3), so that  
30 gradient angle  $\alpha$  may not have to be estimated, calculated or measured by a cost-creating sensor.

Equation (3) solved for estimated value  $\hat{m}$  of the vehicle mass then reads:

$$\dot{\hat{m}} = \frac{\dot{F}}{\dot{a}} \quad (4)$$

Equation (4) thus forms the estimate equation for mass m of the vehicle. The estimate equation may be calculated

5 continuously, e.g., by recursive methods. The recursive algorithms used may contain so-called forget factors with which the behavior of the algorithm may be adjusted. The forget factors are adjusted in the direction of faster convergence in suitable situations, e.g., during longer stand-still times in  
10 which mass m of the vehicle may change.

To estimate m according to equation (4), the variables F and a or  $\dot{F} = dF/dt$  and  $\dot{a} = da/dt$  may need to be determined.

15 Motive force F includes, inter alia, the known running resistance and drive resistance developing, for example, due to friction losses in the engine and transmission, etc., and/or sustained braking forces:

$$F = \frac{M \cdot \omega - \Theta \cdot \dot{\omega}}{v} \cdot \eta - 1/2 p \cdot c_w \cdot A \cdot v^2 \quad (5)$$

20 where

M = Engine torque including friction torque

$\omega$  = Engine speed

v = Vehicle velocity

A = Frontal area of the vehicle

25  $\eta$  = Drive-train efficiency

$\Theta$  = Moment of inertia of the engine

p = Density of the air

$c_w$  = Drag coefficient

30 The quantities in equation (5) therefore include vehicle-specific quantities such as moment of inertia of the engine  $\Theta$ , drag coefficient  $c_w$ , frontal area A and drive-train efficiency  $\eta$  of the vehicle. The vehicle-specific quantities

may be stored in a memory unit of a control unit of the vehicle. Furthermore, equation (5) includes quantities concerning the instantaneous driving conditions of the vehicle such as engine torque  $M$ , engine speed  $\omega$ , vehicle velocity  $v$  and density  $p$  of the ambient air that are measurable or are constantly able to be fetched in the control unit of the vehicle. From the indicated data or quantities, a calculating unit, e.g., the control unit of the vehicle itself, is able to calculate motive force  $F$  and acceleration  $a$ .

The term  $\dot{a}$  in the denominator of equation (4) is the derivation of vehicle acceleration  $a$  with respect to time  $t$  and is referred to as jolt. Therefore, mass  $m$  may only be estimated during suitable phases in which  $da/dt$  and  $dF/dt$  is not equal to 0.

The control unit differentiates quantities  $F$  and  $a$  using suitable methods such as the two-point differentiation method or a state-variable filter, the derivation, e.g., being carried out over longer time intervals. To improve the accuracy of the estimation, the differentiated quantities may subsequently be filtered. For example, using a least-square algorithm, estimated value  $\hat{m}$  for the vehicle mass is calculated as follows:

$$\hat{m} = \frac{\sum_{i=1}^N \dot{F}_i \cdot \ddot{v}_i}{\sum_{i=1}^N \ddot{v}_i \cdot \ddot{v}_i} \quad (6)$$

with  $i$  as subscript for the  $i$ -th measured value. The measured quantities such as vehicle velocity  $v$  are suitably weighted, for example, the weighting being carried out as a function of the accuracy of the measured quantities. Moreover, the measured quantities concerning the instantaneous driving conditions of the vehicle may be filtered as a function of the signal quality. The quantities concerning the instantaneous

driving conditions of the vehicle may furthermore be measured repeatedly; and the measurements weighted differently.

Depending on the quality of the measured quantities for vehicle velocity  $v$  and force  $F$ , instead of calculating  $\hat{m}$ , it may be more favorable to calculate the reciprocal value  $1 / \hat{m}$ . Alternatively, both a value for  $\hat{m}$  and reciprocal value  $1/\hat{m}$  may be calculated, and a weighted average value formed.

- 10 In addition to the method, a device may be for effecting a computer-aided estimation of the mass of a vehicle, , e.g., of a commercial vehicle. This device includes a calculating unit for calculating the mass of the vehicle and/or the reciprocal value of the mass from the equilibrium relationship between  
15 motive force  $F$  and the running resistances, into which mass  $m$  and gradient angle  $\alpha$  of the roadway are entered as calculation quantities, after a computer-aided differentiation of the equilibrium relationship with respect to time, assuming gradient angle  $\alpha$  is constant. This calculating unit may be  
20 integrated into the control unit of the vehicle.